



L&T Construction

Water, Smart World & Communication.

Water & Effluent Treatment - SBG, EDRC,

P.O.BOX - 979, MANAPAKKAM, CHENNAI-600 089, INDIA. PHONE : 044-3384 2085
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DRAWING / DOCUMENT TRANSMITTAL

To Executive Engineer, TWSP Komarambheem-Asifabad Segment, Asifabad Govt. of Telangana.	Date:	28/1/2016.
	Our Ref.:	LE 150883 /04.
	Your Ref.:	
Project	Providing drinking water to habitations in Komarambheem-Asifabad Segment in Adilabad District.	
Subject	Drawings & Documents Submission.	
Kind Attn.	The Executive Engineer, TWSP Komarambheem-Asifabad Segment, Asifabad.	

Please find enclosed the following document / drawings for Approval as listed below.

Sl. No.	Description	Drawing/Document No.	Rev. No.	Qty.	Cat.	Type	Remarks
1	Basic Engineering Package for 30 MLD WTP	LE150883-P-WS-WT-BE-2001	B	1	A	SC	
2	Layout Plan for WTP	LE150883-P-WS-WT-PP-2002	B	1	A	SC	
3	Hydraulic Flow Diagram for 30MLD WTP	LE150883-P-WS-WT-HF-2003	B	1	A	SC	

NOTES:

Sl. No	Distribution	Qty.	Cat.	Type	Remarks
1	The Executive Engineer, TWSP Komarambheem-Asifabad Segment, Asifabad	-	I	SC	
2	EPS - BU Head, HQ.	-	I	SC	
3	SGD - Segment Head (South & East), HQ	-	I	SC	
4	PRH - Cluster Head, HYCO	-	I	SC	
5	RKS - Project Manager	-	I	SC	
6	MBS / BRJ - WS&D, EDRC	-	I	SC	
7	CVR / VVK / RR / VP / RR / RPV - WS&D, EDRC	-	I	SC	
8	RKP / LSV - Electrical & Instrumentation BU	-	I	SC	

CATEGORY (Cat.):

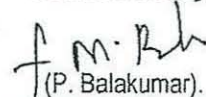
A - For Approval B - As Built
G - Good for Construction I - For Information
P - Preliminary T - For Tender Purpose

Type:

CD - Compact Disc FD - Floppy Disk PR - Prints
RP - Reproducible SC - Soft Copy TR - Tracings
TC - Transmittal Copy ZD - Zip Disk

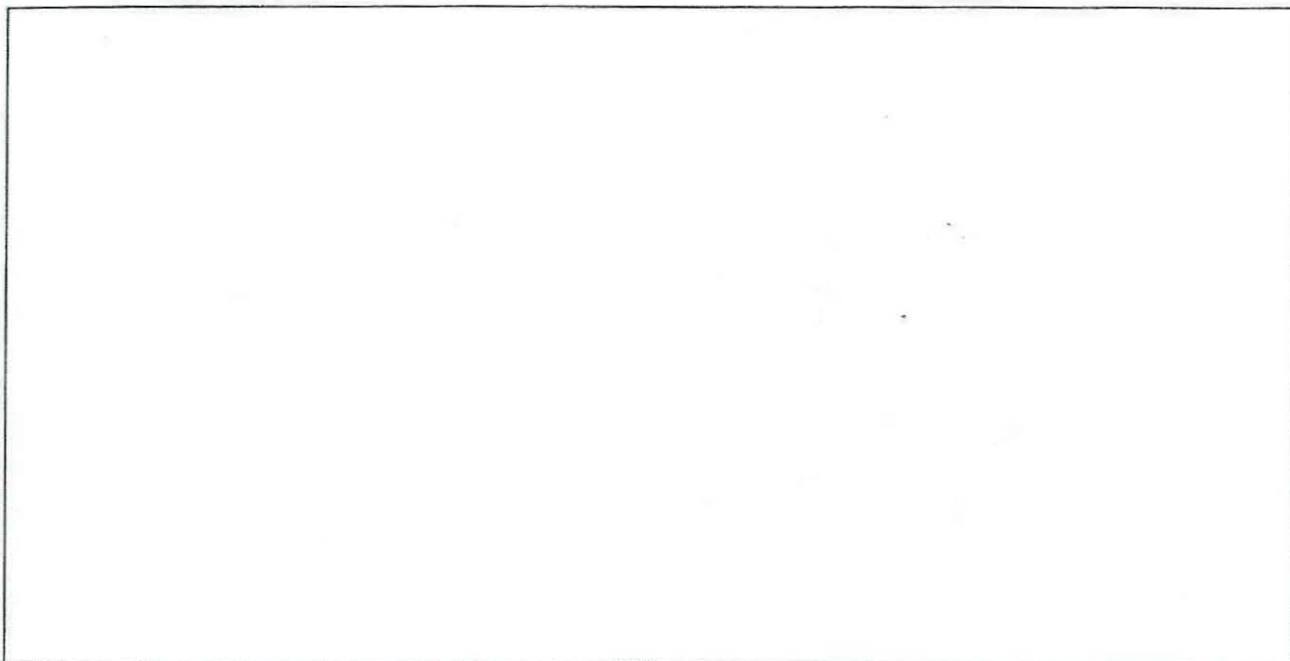
Thanking you and assuring you of our best services at all times.

Yours faithfully,


(P. Balakumar).

Head - EDRC, WET SBG, Water & Effluent Treatment,
L&T CONSTRUCTION.

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28.01.2016	B	As per consultant comments received by mail dtd. 25.01.2016	28.01.2016	28.01.2016	28.01.2016
30.12.2015	A		SRV	VVK	MBS/BRJ
DATE	REV. NO.	DESCRIPTION	Prepared	Checked	Approved
REVISIONS					



L&T CONSTRUCTION
WATER, SMART WORLD & COMMUNICATION

CLIENT : Govt. of Telangana Rural Water Supply & Sanitation Department	CONSULTANT :
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PROJECT :
 Providing drinking water to habitations in KomaramBheem-Asifabad segment in Adilabad district - 30 MLD WTP

SUPPLIER / CONTRACTOR:
 L&T CONSTRUCTION - WATER & EFFLUENT TREATMENT SBG

Job No **LE150883**

	NAME	SIGN	DATE	TITLE : BASIC ENGINEERING PACKAGE FOR 30 MLD WATER TREATMENT PLANT
PRED	SRV	SRV	24.12.2015	
CHKD	VVK	VVK	28.12.2015	
APPD	BRJ	BRJ	30.12.2015	

DOC.No.	L E 1 5 0 8 8 3 - P - W S - W T - B E - 2 0 0 1	SIZE A4	REV. B
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RELEASED FOR	<input type="checkbox"/> PRELIMINARY	<input type="checkbox"/> TENDER	<input type="checkbox"/> INFORMATION	<input checked="" type="checkbox"/> APPROVAL	<input type="checkbox"/> CONSTRUCTION
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Submitted sir,

Sub:RWS&S-TDWSP- Asifabad –30MLD WTP GAD Hydraulic Desings and Hydraulic Flowlevels–
Asifabad segment - Adilabad District- GAD Designs -Approval-Reg.

Kindly persue the GAD ,Hydraulic Designs and Hydraulic flow levels of the following 30MLD Water Treatment Plant at Asifabad submitted by the Executive Engineer TDWSP Asifabad Division Adilabad District for approval.

1. 115 MLD WTP at Asifabad segment

The Executive Engineer TDWSP , Asifabad has submitted GAD ,Hydraulic Designs and Hydraulic flow levels of 30 MLDWTP of Asifabad Segment based on the field conditions and as per the estimate provisions as well as vetted by Wapcos the designs for the above component is verified and submitted for approval .

The following design parameters were considered:

- Capacity : 30 MLD
- Operating Hours : : 22 Hours
- Cascade Aerator : : 6.5 mtr Dia with 4 steps
- Stilliing chamber : : 2.9 mtr x 2.9 Mtr x 3.2 mtr depth
- Flash mixer: : 2.7mtr x2.7 mtr X 3.8 mtr depth
- Clariflocculator Inlet: : 900 mm Dia , DI pipe
- Clariflocculator : : 39 mtr dia
- Filter beds: : 06 no.s - 7.6 mtr x 5.6 mtr
- wash water tank: : 450 kl
- Chemical house: : 10 mtr x 7 mtr
- Chlorine house : : 8 mtr x 5.5 mtr
- Clear water sump : : 24 mtr x 23.6 mtr

As per the above parameters the GAD of the WTP is verified, duly followed by CPHEEO Manual. The Hydraulic Designs and Flow levels proposed are safe and sufficient.

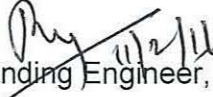
The additional points noted after checking the designs are:

- Based on above GAD and hydraulic Flow levels the EE, TDWSP Asifabad Division is instructed to proceed further for submission of structural Designs.

Subject to approval a draft memo addressed to the EE, TDWSP Asifabad Division , for communicating approved GAD and Hydraulic flow levels is put up for kind perusal and approval.


AEE (Designs)
TDWSP, Nirmal Circle

DEE (Designs)
TDWSP, Nirmal Circle


Superintending Engineer,
TDWSP, Nirmal Circle

GOVERNMENT OF TELANGANA
TELANGANA DRINKING WATER SUPPLY PROJECT
Office of the Superintending Engineer, TDWSP CIRCLE Nirmal

Memo No.AEE/TDWSP/Adilabad-Asifabad/Designs /2016, Dt. - -

Sub: Adilabad District Asifabad Segment - TDWSP - "Providing drinking water to Asifabad segment in Adilabad District from Komarambeem Reservoir under Telangana drinking water supply project (TDWSP) – GAD and Hydraulic Design of 30 MLD WTP, Asifabad - Approval – Reg.

Ref: 1) PR & RD RWS-IV Dept. Memo No 11548/RWS-IV/2015 Dated 04.12.2015

2) SE TDWSP Nirmal Circle agreement no;3/2015-2016 Dated 28.10.2015

3) Proposals submitted by EE TDWSP Asifabad, Dated;11.02.2016

*** **

The Hydraulic Designs, Flow levels and GAD of 30 MLD WTP at Asifabad, Pertaining to the work of Providing Drinking Water to Asifabad Segment of Adilabad district, which has been vetted by WAPCOS, for the following components are approved and herewith communicated for grounding the work.

The details of the components are,

- a) Basic Engineering Package for 30 MLD WTP
- b) Layout Plan for WTP
- c) Hydraulic flow Diagram for 30MLD WTP

Based on above GAD and hydraulic Flow levels the EE, TDWSP Asifabad Division is instructed to proceed further for submission of structural Designs immediately.


Superintending Engineer,
TDWSP Circle, Nirmal,

To

The Executive Engineer TDWSP Asifabad Division for necessary action.

Copy Submitted to the Chief Engineer TDWSP Hyderabad for favor of information

Copy Submitted to the Engineer in chief RWS&S Hyderabad for favor of kind information



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WATER, SMART WORLD & COMMUNICATION

WET SBG

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CONSULTANT	-	Prepared By	Checked By	Approved By Sheet 1
JOB NO	LE150883	TITLE	CONTENTS	SRV/lu VVK BRJ

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ii. Hydraulic Flow Diagram for WTP (Drg.No: LE150883-P-WS-WT-HF-2003)	
iii. Process Flow Diagram (Drg.No: LE150883-P-WS-WT-PF-2004)	

CHAPTER -1

INTRODUCTION



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WATER, SMART WORLD & COMMUNICATION

WET SBG		DRAWING/DOCUMENT NO	DATE: 28.01.2016
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JOB NO.	LE150883	TITLE: INTRODUCTION	SRV <i>f.l.</i> VVK <i>[Signature]</i>

CHAPTER-1

INTRODUCTION

The Telangana Drinking Water Supply Project envisages providing safe, adequate, permanent, sustainable and secured water supply system for covering Rural, Urban and Industrial areas by year 2018 on par with National Rural Drinking Water Supply Guidelines available for Rural Water Supply.

The project objective is to provide safe drinking water at house hold level up to kitchen at the defined and approved norms such that the people need not go to the streets for collection of water from public stand posts or for other modes of facilities.

KomaramBheem Dam is located in Asifabad Mandal of Adilabad district. As this is a dependable source in the vicinity, it is proposed to take water of the Dam as the source for this project.

The water treatment plant of **output capacity of 30 MLD** broadly consists of Cascade Aerator, Stilling Chamber, Pre & Post Chlorination, Parshall flume, Flash Mixer, Chemical dosing systems for alum, Clariflocculator and Rapid Gravity Sand Filters.

The above system has been awarded to Larsen & Toubro, ECC division, Chennai and the scope covers Design, Engineering, Procurement, Supply, Transportation, Construction, Manufacture/Fabrication, Erection, Testing, Painting, Civil work, Mechanical work, electrical work, Piping work, Instrumentation work, Inspection work, Storage at site, Transit & site insurance, Testing & Commissioning, Trial runs and performance guarantee test runs and handling over the entire works on Turnkey basis.

The scope this Basic Engineering and process package is presented in 7 chapters as given in the list of contents and broadly describes various aspects of process and other technical requirements of the water treatment plant.

CHAPTER - 2

PROCESS DESIGN BASIS



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WET SBG		DRAWING/DOCUMENT NO	DATE: 28.01.2016
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CHAPTER - 2

PROCESS DESIGN BASIS

The design, manufacture and performance of the drinking water treatment plant shall be in compliance with the NIT and requirements of Manual of Water Supply, Third Edition 1999 published by the expert committee of Central Public Health & Environmental Engineering Organization, Govt. of India.

The treatment plant scheme shall broadly comprise of coagulation, flocculation, clarification, filtration and disinfection processes for delivering treated water of specified physical, chemical, and bacteriological quality. The design basis considered for the raw water treatment plant is as given below.

The source of raw water is from KomaramBheem Dam in Asifabad Mandal of Adilabad district.

(i). Design output capacity of the plant: **30 MLD**

(ii). The raw water characteristics considered at the inlet of the treatment plant as given below.

1. The raw water characteristics considered at the inlet of the treatment plant are as per the Table-1 and the raw water analysis report attached in **Chapter 6**.

Table -1 (Raw water Quality considered for the design)

Sl. No.	Parameters	Value
1	Turbidity (NTU)	50
2	pH	7.5-8.5
3	Color (Cobalt Scale)	5
4	Total Aluminum	Nil



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2. The treated water characteristics for the following parameters shall be as per NIT Specifications.

Colour - 3 or less on Cobalt scale

Turbidity - Not more than 1 NTU

Suspended Solids - Less than 2.5 mg/l

Total Aluminium - Less than 0.2 mg/l

Taste and Odour - Unobjectionable

Coliform organisms MPN /100ml - Nil.

CHAPTER - 3

TREATMENT PHILOSOPHY



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CHAPTER - 3

TREATMENT PHILOSOPHY

The water treatment plant is designed for Treated Water Output of **30 MLD in 22 hours**. The Hydraulics of the treatment plant is designed in such a way that water flows by gravity from the cascade aerator to the clear water reservoir and the sludge generated from the Clariflocculator and the filter Backwash water will flow by gravity to the nearest drain through pipeline.

Broadly, the flow scheme shall comprise the following process units:

- a) Cascade Aerator
- b) Stilling chamber
- c) Parshall Flume
- d) Flash Mixer
- e) Clariflocculator
- f) Bypass Channel
- g) Rapid Gravity Sand filters
- h) Backwash overhead tank
- i) Chemical house
- j) Chlorination building

PROCESS DESCRIPTION

Broadly the process scheme for the WTP is described below:

The extent of work is to treat raw water from KomaramBheem Dam so as to ensure supply of 30 MLD treated water output @ 22 hours operation.



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Cascade Aerator

The raw water is pumped to the inlet of the water treatment plant i.e. the raw water enters the cascade aerator at the inlet of the water treatment plant. The Cascade Aerator is of circular type of concrete construction with an inlet pipe, located at the center. The aerator shall have number of trays/steps. Water is introduced into the top tray through the central feed pipe and moves down successive trays. Air is naturally introduced to the water in such a way that some iron reduction will occur. A collecting launder shall provide to receive the aerated water falling from the lowest tray.

Design Criteria:

B

No of steps provided - 4 nos

Type -Circular

Surface loading rate - 0.015 m²/m³/hr

Rise between steps - 0.3 m

Stilling Chamber

Stilling chamber is provided to receive the water from cascade aerator and it is provided to avoid the turbulence before the water enters to the parshall flume, where the flow will be measured. The chlorine solution (Pre chlorination) shall be injected by bottom mounted diffuser pipe. This chamber is in R.C.C construction.

Design Criteria:

Retention time - 60 sec

Parshall Flume

Water from the stilling chamber flows through an R.C.C. channel installed with parshall flume of standard design where ultrasonic flow meter is installed to monitor the flow



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through the channel. The alum is dosed at the upstream of the channel. The channel is also installed with Turbidity meter.

Flash Mixer

Flash mixer is provided for mixing of alum chemicals and shall be of RCC Construction. Alum is dosed at the upstream of the flash mixer and the tank is installed with agitator for uniform distribution of the chemicals through the water. Chemically mixed water from the flash mixer will flow to the Clariflocculator.

Design Criteria:

No of mixer provided -1 No.

Retention time - 60 sec

Clariflocculator

Clariflocculator is provided with combined coagulation and sedimentation processes effectively taking place in a single unit. The water, flash mixed with chemicals, is fed in the circular flocculation compartment, which is built at the centre and fitted with slowly revolving paddles of 2nos. which rotate on their vertical axis. The Clariflocculator arrangement is based on a central feed, flocculation and clarification. The flocculated water passes out from the bottom of the flocculation tank to the concentric outer clarifying zone, through a wide opening and the suspended particles will settle to the bottom of the clarifier and the clarified water overflows into the peripheral launders with Submerged Orifices through clarified water channel. The flocculation as well as clarification zones are served by inwardly raking rotating blades, hanging from the peripheral driven moving bridge so that the settled sludge is mechanically scraped and will flow by gravity to the nearest Drain.

Design Criteria:

No of Clariflocculators provided -1 No.



Surface loading rate - 40 m³/m²/day



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Retention time - < 2.5 hrs

Bypass Channel

One RCC channel is provided from Flash Mixer to the filter inlet channel to bypass the Clariflocculator if required. This Filter inlet channel will lead to the rapid sand gravity filters.

Rapid Gravity Sand Filters

The clarified water from clarified water channel or from the bypass channel enters into the filter inlet channel. It is then routed to the rapid gravity filters (declining rate type with manifold and Lateral for under drainage system). Filtration shall be by gravity downwards through a bed of filter sand. The filtered water is collected through the under drain system and flows into an outlet chamber and into the common filtered water channel. The dirty backwash water from filters shall be disposed to the nearest drain.

Design Criteria

No of Filters - 6 nos

Filtration rate - 5.5 m/hr

Type -Declining rate type

Back Wash Tank

When the filter head loss increases due to clogging of the bed, the filters shall be taken on back washing using air and water. There overhead backwash water storage tank sized for two filter washes will deliver the backwash water to filters. The backwash storage tank shall be filled by centrifugal pumps which will take the water from the filtered water channel.

Clear Water Reservoir

The filtered water from the filtered water channel is taken through the channel, which leads upto Clear water Reservoir.



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Chemical House

The chemical house is provided for the necessary space for 90 days storage of chemicals.

Alum is used as a coagulant in the removal of raw water turbidity upto maximum 50ppm of dosage of alum is considered as 30 ppm for design.

A two storied chemical house of RCC structure with access to the first floor by means of stairs. Adequate area as per contract requirement shall be provided for the following:

Ground Floor:

- Chemical storage in ground floor for 90 days requirement for an average dosage of 20ppm.

First Floor:

- Chemical dosing tanks (2 nos) and dosing pumps (1W+1S) is provided.

Chlorination Building

Chlorine shall be dosed as disinfectant to eliminate algae and other microbial growths from the water. Pre chlorination in the stilling chamber is found to remove colour, odour & taste and chlorine will also oxidize iron & manganese which is present in raw water.

Post chlorination is to be done at filtered water outlet.

Chlorination building is designed for considering two month storage of chlorine drums.

Pre Chlorinators: 2 Nos (1W+1S)

Post Chlorinators: 2 Nos (1W+1S)

Type: Vacuum

Dosage: 5 ppm for Pre chlorination & 5 ppm for Post chlorination.

Storage: 5 ppm for Pre chlorination & 2 ppm for Post chlorination.

CHAPTER - 4

PROCESS DESIGN

CALCULATION



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WATER, SMART WORLD & COMMUNICATION

WET SBG

PROCESS DESIGN CALCULATIONS- 30 MLD WTP FOR KOMARAMBHEEM-ASIFABAD SEGMENT

PROJECT	Providing drinking water to habitations in KomaramBheem-Asifabad segment in Adilabad district - 30 MLD WTP	DRAWING/DOCUMENT NO	DATE	28.01.2016		
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References:

1. Contract document of KomaramBheem-Asifabad segment in Adilabad district
2. CPHEEO Manual on water supply and Treatment, May 1999 Edition
3. IS 14371-1996. Measurement of Liquid flow in open channels - Parshall and Saniri flumes

The design, manufacture and performance of the Water Treatment plant (WTP) shall be in compliance with the requirements of Manual on Water Supply and Treatment, Third Edition 1999 published by the expert Committee, Central Public Health & Environmental Engineering Organisation, Govt. of India and relevant BIS codes of practice.

Basic Design criteria

Inlet Design Capacity	31.58 MLD
No of hours of operation	22 hours
Raw Water Quality	As per Table-1 in Chapter 2 & Chapter 6
Treated Water Quality	As per Chapter 2

Design flow

Outlet Capacity of WTP as per Contract specification	30	MLD
Outlet Flow in terms of cum/hr	1363.64	m ³ /hr
Inlet capacity of WTP with considering 5% losses	31.58	MLD
Flow in terms of cum/hr	1435.41	Cum/hr.
Flow in terms of cum/sec	0.40	Cum/sec.
Channels, conduits with 20% Overloading	1722.49	m ³ /hr

Design Criteria

- Cascade Aerator : Cascade aerator is designed by considering a surface loading area of 0.015 m²/m³/hr
- Stilling Chamber : It is designed considering a detention time of 60 s .
- Parshall Flume : Designed as per IS code : 14371:1996 " Measurement of Liquid flow in open channels"
- Flash Mixer : Flash mixer is designed by considering a detention time of 60 s
- Clariflocculator : Clariflocculator is designed by considering SLR 40 m³/m²/day
- Gravity Filters : Filters are designed considering filtration rate of 5.5 m³/m²/hr during normal flow rate with all filters in operation (declining rate)
- Alum dosing : Alum Mixing tanks are designed for Maximum dosage of 30ppm & Storage for average dosage of 20 ppm
- Chlorination : Pre & Post chlorination designed for dose of 5.0 ppm & storage of 5 ppm for Pre & 2 ppm for Post chlorination.

All channels including Bypass channel are designed for 20 % Overloading .

1.Cascade aerator

Design flow	1435.41	m ³ /hr
No of cascade aerator provided	1.00	no
Flow per cascade aerator	1435.41	m ³ /hr
Diameter of influent pipe	0.70	m
Diameter of the inlet bell mouth dia	1.00	m
Area of the bell mouth	0.79	m ²
Number of steps considered	4	nos

B



WET SBG

PROCESS DESIGN CALCULATIONS- 30 MLD WTP FOR KOMARAMBHEEM-ASIFABAD SEGMENT

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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV
			VVK	BRJ

	Size of tread considered		0.70 m	
	Rise/spacing between steps		0.3 m	
	Total Height of Fall		1.2 m	
	Surface loading rate considered		0.015 m ² /m ³ /hr	
	Total Area Required		21.53 m ²	
	Total area required including bell mouth		22.32 m ²	
	Diameter of the Bottom Most Step		5.4 m	
	Total Area Provided		22.91 m ²	
B	Size of Collection Launder			
	Flow in Launder at Normal Condition		717.70 m ³ /hr	
	Velocity in Launder considered		0.70 m/s	
	Cross Section Area		0.28 m ²	
	Width of the Launder Considered		0.55 m	
	Side Water Depth/Height		0.5 m	
	Free Board in Launder		0.30 m	
	Flow in Launder at 20% Overloading Condition		861.24 m ³ /hr	
	Velocity in Launder considered		0.90 m/sec	
	Cross Section Area		0.27 m ²	
	Width of Launder considered		0.55 m	
	Side Water Depth/Height		0.49 m	
	Side water Depth considered		0.50 m	
	Free Board in Launder		0.30 m	
	SIZE:	W(m)	LD (m)	FB (m)
	Launder Size:	0.55	0.50	0.30
B	At normal flow condition the velocity of the launder is 0.7m/s and at overloading condition the velocity is 0.9m/s.			
B	<u>Diameter of each Cascade provided inclusive of Central Influent Pipe</u>			
	Diameter of the 1st cascade		1.2 m	
	Diameter of the 2nd cascade		2.6 m	
	Diameter of the 3rd Cascade		4.0 m	
	Diameter of the 4th Cascade		5.4 m	
	Diameter of Cascade aerator including launder		6.5 m	



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SIZE:	Dia (m)	H (m)	Steps nos.	Tread (m)	Rise (m)
Aerator Size:	5.40	1.2	4.0	0.7	0.3

2. Stilling Chamber					
No. of Units					1 nos. ✓
Total Design flow					1435.4 m ³ /hr
					0.40 m ³ /s ✓
Detention time considered					60 s ✓
Volume of the chamber required					23.94 m ³
Liquid depth considered					2.9 m ✓
Area of stilling chamber required					8.26 m ² ✓
Length of chamber required					2.87 m ✓
Length of chamber considered					2.9 m ✓
Width of chamber required					2.9 m ✓
Volume of the chamber provided					24.39 m ³ ✓
Free Board in chamber					0.3 m ✓

SIZE:	L (m)	W (m)	LD (m)	FB (m)
Chamber Size	2.9	2.9	2.9	0.3

3. Raw Measuring channel with Parshall Flume					
No. of Channel					1.00 No ✓
Velocity through channel is considered as					0.50 m/s ✓
Normal Flow to the channel					0.40 m ³ /s ✓
Flow with 20% overloading					0.48 m ³ /s ✓
Area of channel required					0.96 m ² ✓
Channel depth considered					0.80 m
Width of channel required					1.2 m ✓
Width of the channel provided					1.2 m ✓
Free Board in channel					0.3 m

SIZE:	W(m)	LD (m)	FB (m)
Channel Size:	1.20	0.80	0.30



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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV <i>f.b</i>	VVK <i>[Signature]</i> BRJ										
Parshall Flume															
Reference:															
IS 14371:1996:" Measurement of Liquid Flow in Open channels - PARSHALL and SANIIRI FLUMES"															
Flow to the Parshall flume				0.48	m ³ /s ✓										
As per Table 3 and Table 4 of IS 14371,1996 , for parshall flume no. 4															
Hence as per the code,															
Width of flume				1020	mm ✓										
Throat width for parshall flume				450	mm ✓										
4. Flash Mixer															
No. of Units provided				1	no.										
Design flow per unit				1435.41	m ³ /hr ✓										
				i.e	0.40	m ³ /s									
Detention time considered				60	s										
Volume required				23.92	m ³ ✓										
Liquid depth considered				3.5	m										
Area of flash mixer required				6.84	m ² ✓										
Length & Width of Flash mixer required & provided				2.7	m ✓										
Volume of the flash mixer provided				25.52	m ³ ✓										
Free board in tank				0.3	m ✓										
<table border="1"> <thead> <tr> <th>SIZE:</th> <th>L (m)</th> <th>W (m)</th> <th>LD (m)</th> <th>FB (m)</th> </tr> </thead> <tbody> <tr> <td>Tank Size</td> <td>2.7</td> <td>2.7</td> <td>3.5</td> <td>0.3</td> </tr> </tbody> </table>						SIZE:	L (m)	W (m)	LD (m)	FB (m)	Tank Size	2.7	2.7	3.5	0.3
SIZE:	L (m)	W (m)	LD (m)	FB (m)											
Tank Size	2.7	2.7	3.5	0.3											
Detention time with 20% overloading				53.33	secs										
As per CPHEEO Manual, detention time for Flash Mixer shall range from 30-60 s				Hence O.K											
5. Clariflocculator															
Flocculator															
Total design flow				1435.41	m ³ /hr ✓										
No.of Units				1	Nos.										
Design flow capacity per Unit				1435.41	m ³ /hr ✓										
Flocculation zone of Clariflocculator															
B	Retention time considered				30	min ✓									
	Volume of flocculator required				717.7	m ³ ✓									
	Side water depth considered				3	m ✓									
	Plan area required for the flocculator				239.23	m ² ✓									



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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV <i>f.u.</i>	VVK <i>H</i>
	Velocity through central column is considered as			0.6 m/s	✓
	Inside dia of central column arrived			1 m	
	Consider wall thickness for central column and flocculator wall as			0.2 m	
	Outer dia of Central column			1.4 m	✓
	Area for the central column :			1.54 m ²	✓
	Total area required for flocculator including central pipe =239.23+1.54=			240.77 m ²	
B	Inside Diameter of the flocculator required			17.51 m	
	Inside Diameter of the flocculator provided			17.60 m	✓
	Plan area for the flocculator			243.28 m ²	
	Volume of flocculator required			729.84 m ³	✓
			say	730 m ³	✓
	Assume thickness of partition wall			0.3 m	✓
	Flocculator outside Dia =17.6 + 2 x 0.3			18.2 m	✓
	Area of flocculator including walls			260.02 m ²	✓
	Volume provided in the flocculator including walls			780.06 m ³	✓
	Size of Flocculator:	Inside Dia. (m)	LD (m)	FB (m)	
		17.6	3.0	0.3	
	Clarifier:				
B	Surface Loading rate at rated capacity considered			40.0 m ³ /day/m ²	✓
			i.e	1.67 m ³ /hr/m ²	✓
	However provided SLR			1.67 m ³ /hr/m ²	
	Clarifier Area required : (1435.41/1.67)			861.2 m ²	✓
	Total Area of clariflocculator required = 861.2+260.02			1121.22 m ²	
	Dia of clariflocculator			37.8 m	✓
	Provide dia of clariflocculator as			39.0 m	✓
	Size of Clariflocculator : 39 m Dia x 3 m SWD + 0.3 m F.B				
	Area provided for clarification			933.96 m ²	
	Detention time for Clariflocculator			2.8 hrs	✓
B	Note: The actual Surface Loading Rate for the provided dia. of Clariflocculator is 37 m ³ /day/m ²				
	Opening Port				
	Consider velocity in port			0.6 m/s	✓
	Total area of port = 1435.41/3600/0.6			0.67 m ²	✓
	Considering 4 nos of ports, area of each port			0.17 m ²	✓
	Assume width of port			0.45 m	



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CONSULTANT			Prepared By	SRV	Checked By	VVK	
JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV	f/a	Approved By	BRJ
	Depth of port				0.38	m	
	Provided depth of port				0.4	m	
	Provide 4 ports of size 0.45 m (W) X 0.40 m(H)						
	Clariflocculator launder sizing						
	Flow to Clariflocculator Launder with 20% overloading				1685.45	m ³ /hr	
	Flow to one half of the launder = 1685.46/2=				842.73	m ³ /hr	
					0.24	m ³ /s	
	Velocity considered				0.75	m/s ✓	
	Area of the flow				0.31	m ²	
	Width of the launder considered				0.6	m ✓	
	Liquid depth arrived				0.55	m ✓	
	Size of the clariflocculator launder						
	0.6 m (W) x 0.55 m L.D						
	Clariflocculator overflow arrangement (Submerged orifice hole arrangement)						
	Flow with 20% overloading				1685.45	m ³ /hr	
	Velocity considered for sizing of orifices				0.21	m/s ✓	
	Hence, total area of orifice holes required				2.2294	m ² ✓	
	Diameter of each orifice hole considered				63	mm ✓	
	Hence cross-sectional area of each orifice hole				0.00312	m ²	
	Hence total no. of orifices required				716.00	Nos. ✓	
	Wetted perimeter of one orifice hole				0.20	m ✓	
	Total wetted perimeter = Total weir length				141.71	m ✓	
	Actual weir loading rate obtained				11.89	m ³ /hr/m ✓	
		Less than			12.5	m ³ /hr/m ✓	
					Hence O.K		
	Peripheral Diameter of launder				117.81	m ✓	
	Hence C-C distance between orifice holes required				164.5	mm ✓	
	6. Bypass Channel / Clarified Water Channel						
	Flow in Channel at Normal Condition				0.40	m ³ /s	
	Velocity through channel considered				0.7	m/s	
	Area				0.56	m ²	
	Liquid Depth				0.75	m ✓	
	Width of the channel				0.75	m	
	Free board in channel				0.30	m	

B



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CONSULTANT				Prepared By	Checked By	Approved By
JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV f.u	VVK	BRJ
Flow in Channel at 20% Overloading Condition					0.48	m ³ /s
Velocity through channel considered					0.90	m/s
Area					0.53	m ²
Liquid depth (LD)					0.75	m
Width of channel required					0.71	m
Width of channel provided					0.75	m
Free board in channel					0.30	m
SIZE:		W (m)	LD (m)	FB (m)		
Channel Size:		0.75	0.75	0.30		
B	At normal flow condition the velocity of the channel is 0.7m/s and at overloading condition the velocity is 0.9m/s.					
	<u>7. Filter Inlet Channel</u>					
No of channels					2	nos ✓
Normal Flow into the channel					0.20	m ³ /s ✓
Flow into channel with 20% overloading					0.23	m ³ /s ✓
Velocity through channel considered					0.41	m/s ✓
Area					0.57	m ² ✓
Width of channel considered					0.40	m ✓
Liquid depth required					1.43	m ✓
Liquid depth provided					1.45	m ✓
Freeboard in channel					0.30	m ✓
SIZE:		W(m)	LD (m)	FB (m)	No of Channel	
Channel Size:		0.40	1.45	0.30	1.0	
<u>8. Rapid sand Gravity filters</u>						
Type of filter					Declining rate	
Input flow to the filter					1404.55	m ³ /hr ✓
No. of Twin Bed Filters					6	nos ✓
Design flow per bed					234.09	m ³ /hr ✓
Rate of filtration considered					5.5	m/h ✓
Area of filtration required					42.56	m ² ✓
Length of twin bed filter considered					7.60	m ✓
Length of one bed					3.80	m ✓
Width of each bed required					5.6	m ✓



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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV	VVK	BRJ
Width of the bed provided						5.6 m ✓
Length to Width ratio provided						1.36 ✓
<i>As per CPHEEO clause 7.6.3.5 the L/B ratio of filter bed shall be 1.11 to 1.66 averaging about 1.25 to 1.33</i>						
Area of each twin bed filter provided						42.56 m ² ✓
Rate of filtration adopted						5.50 m/hr ✓
Central Gullet width of filter bed						1 m ✓
Filtration rate when 1 filter is taken out for backwashing						6.6 m/h ✓
	SIZE of (Twin Bed)	L (m)	B (m)	Area of bed (m2)	Total No of beds	
		7.60	5.6	42.56	6	
	SIZE of (Single Bed)	L (m)	B (m)	Area of bed (m2)		
		3.80	5.6	21.28		
9. Filter Gates & pipe size						
(i) Filter Inlet gate size						
Flow to each filter with filtration rate of 8.5m/hr.						361.8 m ³ /hr
						0.10 m ³ /sec
Velocity considered						1.00 m/sec
Area						0.10 m ²
						0.32 m
Inlet gate size provided						350*350 mm ✓
(ii) Filter Outlet valve size						
Flow from each filter with filtration rate of 8.5m/hr.						361.8 m ³ /hr
						0.10 m ³ /sec
Velocity considered						0.90 m/sec
Area						0.112 m ²
Dia						0.377 m ✓
Filter Outlet Valve size provided						400 mm
(iii) Backwash Inlet valve size						
Backwash flow						638.4 m ³ /hr
						0.177 m ³ /sec
Velocity considered						3.50 m/sec
Area						0.05 m ²



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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV /-a	VVK /p BRJ
	Dia			0.254 m	
	Backwash inlet valve size provided			300 mm ✓	
	(iv) Backwash Outlet Gate			300	
	Backwash flow			638.4 m ³ /hr	
				0.18 m ³ /sec	
	Velocity considered			1.80 m/sec	
	Area			0.10 m ²	
				0.314 m	
	Backwash outlet gate size provided			350 x 350 mm ✓	
	Filter Media Specifications				
	Depth of sand bed provided			600 mm ✓	
	Depth of gravel			300 mm ✓	
	The depth of water over the top of sand media			1.70 1.80 m ✓	
	Estimation of sand depth (Ref : Page 634 of CPHEEO Manual May 1999 Edition)				
	Assume the depth of sand as 600mm and effective size of sand as 0.6mm				
	The sand depth can be checked against break through of floc through sand bed by				
	calculating minimum depth required using Hudson formula				
	$Qd^3/l = 39323 B$				
	Q : Rate of filtration in m ³ /m ² /hr				
	: 11 m ³ /m ² /hr considering 100% overloading of				
	filter under exigencies				
	d : Sand size in mm - 0.6mm (Mean diameter)				
	h : Terminal head loss in M - 2.5M				
	(Under exigency condition)				
	B : Break through index, 4×10^{-4} considered for poor				
	response to filtration and average degree of pre treatment				
	Therefore Sand depth (l) =			0.51 mm	
	Hence Assumed depth of 600 mm is sufficient to avoid breakthrough of floc				
	Depth of sand provided			0.60 m ✓	
	Depth of gravel provided			0.40 0.30 m ✓	
	Total depth of filter media provided			1.0 0.90 m	



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				VVK <i>VVK</i>
				BRJ

10. Under drain system (Manifold & Laterals)

Plan area of the filter	21.28 m ²
Total area of perforations (0.3% of filters)	0.06 m ²
Size of perforations	12 mm
Total no. of perforations	564.78 Nos.
	say 566 Nos.
Total c/s area of laterals	1787.60 cm ²
Area of central manifold	2681.4 cm ²
	58.43 cm
	0.63 m
Central manifold of 630 mm dia HDPE pipe	
Assume spacing of laterals	20 cm
No. of laterals required	56.00 Nos.
No. of laterals provided	56.00 Nos.
c/s area of laterals	31.9 cm ²
Dia of laterals	6.38 cm
Provided dia of laterals	75 mm

11. Back Wash Water Overhead Tank

Rate of Back wash Flow considered for overhead tank sizing	30.00 m ³ /hr/m ²
Tank designed for considering one filter backwash volume	
Area of one twin bed	42.56 m ²
Backwash water flow rate required for one twin bed	1276.9 m ³ /hr
Duration of Back wash considered for water	10 min
Backwash water flow rate required with water for one twin bed	212.81 m ³
Total volume of backwash water required for two filter beds	425.6 m ³
Water required for miscellaneous purposes like chemical dilution, flushing etc.	21.3 m ³
Hence total Backwash tank volume considered as	446.9 m ³
Consider Liquid depth of backwash water tank as	3.00 m
Area of the Tank	148.97 m ²
Hence diameter of the Tank required	13.77 m
Diameter of the Tank provided	13.8 m
Area of the tank provided	149.57 m ²
Free board	0.30 m
Volume of Tank Provided	449 m ³



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Backwash tank shall be provided as an independent structure

Size of tank	Diameter (m)	Liquid Depth (m)	F.B (m)
	13.8	3.0	0.30

12. Filter BackwashingAir Backwash

No. of blowers considered	2 nos.
No. of working blowers	1 nos.
Area of each half of filter bed	21.28 m ²
Rate of Air Backwash	40 m ³ /hr/m ²
Air Flowrate required	851.2 m ³ /hr @ 0.35 kg/cm ²
Air flowrate provided	900.0 m ³ /hr @ 0.35 kg/cm ²
Velocity in air wash pipe	25 m/sec
Area of pipe Required	0.01 sqm
Diameter of air wash pipe required	0.113 m
Provided diameter of air pipe	150 mm ✓

Backwash Water Pumps

Backwash Pumps considered separately to fill the Backwash Tank	2 nos. ✓
No. of working pumps	1 no.
Capacity of each Backwash pump provided in two hrs to fill the tank	224.4 cum/hr
Pump capacity provided	225.0 m ³ /hr
	at tentative head 20.00 m ✓

Backwash Trough

Rate of flow of backwash	30.00 m ³ /m ² /hr ✓
Backwash water discharge from one half of bed	638.4 m ³ /hr ✓
	0.09 m ³ /sec
Trough Space assumed	1.60 m
No of troughs	4.00 Nos ✓
Discharge per trough	0.02 m ³ /sec
Backwash water discharge $Q = 1.376bh^{1.5}$	
Assume width of trough, 'b' as	0.20 m ✓
Depth	0.187 m ✓
Total depth provided is	0.30 m




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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV <i>flu</i>	VVK <input checked="" type="checkbox"/>	BRJ
	Trough size provided			0.2 mW x 0.30 m Ht		
	13. Dirty Backwash Channel					
	Dirty Backwash Flow to the channel			638.4	m ³ /hr	
	Total flow for which the Dirty Backwash Channel has to be sized			638.4	m ³ /hr	
				0.18	m ³ /sec	
	Velocity considered			1.50	m/sec	
	Area of Channel required			0.12	m ²	
	Considering width of Channel			0.40	m	
	Depth of Channel			0.30	m	
	Depth of Channel provided			0.30	m	
	Freeboard in channel			As per HFD m		
	SIZE:	W(m)	LD (m)	FB (m)		
	Channel Size:	0.40	0.30	As per HFD		
	DirtyBackwash Water from Channel will be disposed to near by drain.					
	14. Filtered Water Channel					
	Flow in channel at Normal Condition			1363.64	m ³ /hr	
	Flow through Channel			0.38	m ³ /s	
	Velocity considered			0.7	m/s	
	Area of the channel			0.53	m ²	
	Width of the channel			0.75	m	
	Depth of the channel			0.7	m	
	Free board in channel			0.30	m	
	Flow in channel at 20% Overloading Condition			1636.36	m ³ /hr	
	Flow through Channel			0.45	m ³ /s	
	Velocity Considered			0.90	m/sec	
	Area of Channel			0.51	m ²	
	Width of Channel			0.75	m	
	Depth of Channel			0.67	m	
	Depth of Channel provided			0.70	m	
	Free board in channel			0.30	m	
	SIZE:	W(m)	LD (m)	FB (m)		
	Channel Size:	0.75	0.70	0.30		



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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV <i>f.a</i>	VVK <i>[Signature]</i> BRJ
B	At normal flow condition the velocity of the channel is 0.7m/s and at overloading condition the velocity is 0.9m/s.				
	15. Chemical House				
	Alum dosage				
	Alum dosage rate			30	mg/l
	Alum requirement per day			947.40	Kg/day
	Alum requirement per hour			43.1	Kg/hr
	Strength of Alum solution			10.00	%
	Volume of 10% Alum solution required			0.43	m ³ /hrs
	Detention Time			12.00	Hrs ✓
	Volume required for 12 hours capacity			5.20	m ³
	Liquid Depth considered			1.75	m
	Free Board considered			0.30	m
	Plan area required			2.97	m ²
	Length and Width of the Tank (Square Tank)			1.72	m
	Length of the Tank			1.75	m
	Width of the Tank			1.75	m
	No. of Tanks			2	Nos ✓
	Size of tank:	L (m)	W (m)	LD (m)	FB (m)
		1.75	1.75	1.75	0.30
	Alum Storage Area Required :				
	Alum reqd. (100 %) for one day at 22 hours operations (Consider 20 ppm)			631.58	Kg/day ✓
	Alum reqd. (100 %) for 90 days at 22 hours operations			56842	Kg /3 month
				56.80	Tonnes ✓
	Considering bulk density of Alum : 1.1 T / m ³			51.60	m ³
	Storage area required for stack ht. of 2 m			25.80	m ²
	Three months storage area provided			26.00	m ² ✓
	Dosing System for Alum:				
	No of Pumps : 2 (1W+1S)			2	Nos (1W+1S) ✓
	Capacity of Alum Dosing Pump required			430.0	LPH@ 20 m head ✓



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PROCESS DESIGN CALCULATIONS- 30 MLD WTP FOR KOMARAMBHEEM-ASIFABAD SEGMENT

PROJECT	Providing drinking water to habitations in KomaramBheem-Asifabad segment in Adilabad district - 30 MLD WTP	DRAWING/DOCUMENT NO	DATE	28.01.2016
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JOB NO	LE150883	TITLE	PROCESS DESIGN CALCULATIONS	SRV /A VVK BRJ

16. Chlorination			
Pre Chlorination			
Flow rate considered		1435.41 m ³ /hr	✓
Max. Dose of chlorine considered		5 mg/L	
Quantity of chlorine reqd. per hr.		7.2 kg/hr	
Therefore capacity of chlorinator provided		8.0 kg/hr	
No. of Chlorinator		2.0 nos.	
No. of Chlorinator Provided (working)		1.0 nos.	
No. of Chlorinator Provided (stand by)		1.0 nos.	
Chlorine required for 60 days of Pre Chlorination for average dose of 5.0 mg/L		9473.68 kg/ for 2 month	✓
Post Chlorination			
Flow rate considered		1353.64 m ³ /hr	
Max. Dose of Chlorine considered		5.0 mg/L	
Quantity of Chlorine reqd. per hr.		6.8 kg/hr	
Capacity of each Chlorinator		7.0 kg/hr	
No. of Chlorinator Required		2.0 nos.	
No. of Chlorinator Provided (working)		1.0 nos.	
No. of Chlorinator Provided (stand by)		1.0 nos.	
Chlorine required for One month of post chlorination for average dose of 2.0 mg/L		3600 kg/for 2 month	
Total Chlorine required for 60 days considering average dose of 5.0 mg/l for Pre & 2.0 mg/l for Post Chlorination		13073.68 kg	
Assuming 930 kg per tonner, no of tonners required		14 nos	
Hence no.of tonners to be provided		14 nos	
No of tonners in one row		7.0 nos	✓

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CHAPTER - 5

HYDRAULIC CALCULATIONS



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HYDRAULIC CALCULATIONS-30 MLD WTP ASIFABAD SEGMENT IN ADILABAD DISTRICT

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In this Chapter hydraulic flow calculations have been carried out to fix the hydraulic levels of various units to ensure smooth gravity flow of water from Cascade aerator to Clear Water Reservoir

REFERENCES :

1. Layout Plan for WTP (Drawing No. -LE150883-P-WS-WT-PP-2002)
2. CPHEEO - Manual on Water Supply and Treatment , May 1999 Edition
3. Top Water Level (TWL) of Clear Water Reservoir is taken as 279.36 m
4. Levels shall be transferred to Hydraulic Flow Diagram of WTP (Dwg No. LE150883.-P-WS-WT-HF-2003)
5. Two levels of FGL 279.5 & 280 considered for the Water Treatment Plant.

A) Following formula is used for arriving head loss due to fittings :

$$H_{i(f)} = KV^2 / 2g$$

Where,

- K = Resistant co-efficient
V = Velocity of flow in m/sec
g = Acceleration due to gravity in m/sec² = 9.81 m/sec²

The 'K' factor for valves and fittings are taken from CPHEEO manual

B) For gravity flows in open channels / circular conduits Manning's formula shall be used for arriving Head loss

$$V = 1/n \times R^{2/3} \times S^{1/2}$$

- Where, V = Velocity of flow in m/sec
n = Manning's co-efficient of roughness
R = Hydraulic radius in m
S = Slope of hydraulic gradient

Top water level (TWL) of CWR is taken as 279.36 m

As per clause 6.2.2 of CPHEEO Manual on Water Supply & Treatment, For general design purposes the Manning's co-efficient value of all sizes may be taken as of 0.013 for plastic pipes / 0.015 for other pipes /
RCC channel - 0.014

C) Discharge through a rectangular weir is calculated by

$$Q = \frac{2}{3} C_e \sqrt{2gbe} H^{1.5}$$

where,



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be = effective width = Actual width of weir (b) + K (Value of k being 2.5 mm, 3 mm and 4 mm for b/B ranges of upto 0.4, 0.4 to 0.6 and 0.6 to 0.8 respectively)

b/B = ratio of the width of the notch to the width of the channel

H = effective head = actual head measured (h) + 1 mm

g = acceleration due to gravity

C_e = varies from 0.58 to 0.7 for values of b/B from 0 to 0.8

D) Flow through pipes can be calculated by Modified hazen Williams Formula

$$h = [1.49 \left(\frac{Q}{C_p} \right)^{1.851} / 994.62 D^{4.871}]$$

Where,

V = Velocity of flow in m/s;

C_p = pipe roughness coefficient; (1 for smooth pipes; <1 for rough pipes)

r = hydraulic radius in m;

s = friction slope;

D = internal diameter of pipe in m

h = friction head loss in m

L = length of pipe in m; and

Q = flow in pipe in m³/s.

E) A following formula is used for arriving Head loss due to Launder

Critical depth at the end of Launder

$$y_2 = (q/b)^{2/3} / g^{1/3}$$

Liquid depth at the upper end of the Launder

$$y_1 = y_2^2 + (2[q' LN] / (GB^2 y_2))^{1/2}$$

Following K Values are used for arriving head loss

Entrance Shape well rounded	0.50
Sudden Contractions	0.3 - 0.5
90 deg. Bend	0.75
45 deg. Bend	0.4 - 0.75
Tee 90 deg. Take off	1.50
Coupling	0.30
Gate valve	0.3 - 0.4
Butterfly valve	0.30
Orifice plate	1.00
Globe valve	10.00
Ball valve	0.50
Check valve	2.50
T-Type strainer	2/3.5



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CONSULTANT				Prepared By	SRV /ll	Checked By	VVK /ll
JOB NO	LE150883	TITLE	HYDRAULIC CALCULATIONS	Approved By	BRJ		
	Diaphragm valve						2.30
	Sluice gate						0.62
	Entry to pipe						0.50
	Exit to pipe						1.00
1 Head loss between Filtered Water pipe to Clear Water Reservoir (CWR)							
	Top water level (TWL) of CWR is taken as						279.36 m
							$h = [L(\frac{Q}{Cr})^{1.81}] / 994.62 D^{4.81}$
	c). Head Loss in Filtered water channel (FWC):						
	Design flow in filtered water channel						1636.36 m ³ /hr.
	Channel size selected						
					Width of channel		0.75 m
					Liquid depth of channel		0.70 m
	Velocity of water						0.9 m/s
	Length considered for head loss (as per layout)						68 m
	Using Manning's formula , n for concrete						0.014
					Slope,S		0.00059
					Loss of head		0.04 m
	Losses due to 90 deg. Bend				$h=kv^2/2g$		0.03 m
					Total no of bend		1.00 no
					Total loss due to all bend		0.03 m
	Total losses						0.10 m
	Provided free fall of 0.3m						0.30 m
	Total losses between filtered water channel to CWR provided						0.4 m
	TWL of Filtered Water Channel						279.76 m
	Depth of the Filtered Water Channel						0.70 m
	Invert level of Filtered Water Channel						279.06 m
2 Head Loss between filter control chamber & filter water channel							
a. Head loss between filter control chamber and FWC provided with weir arrangement							
	Flow over the weir						0.08 m ³ /s
	Width of the weir						1.00 m
	Head over the Weir [Q = (2/3) C L (2g) ^{0.5} H ^{1.5} , where C=0.624]						0.12 m
	Head over the weir						0.12 m
	However, TWL at filter control chamber provided is						280.13 m
	Depth of Filter Control Chamber						1.0 m
	Invert level of Filter Control Chamber						279.13 m
	Provided free fall of 0.15m from FWC to weir						0.15 m
	Weir Crest Level						280.01 m



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b. Head loss due to 90° bends

Consider pipe dia as 400 mm

Velocity of flow 0.8 m/s

$h = kv^2 / 2g$

$h = 0.75 \times 0.8^2 / (2 \times 9.81)$ 0.025 m

No. of bends 2 nos

Total loss of head 0.05 m

Head loss due to pipe entry

Pipe size considered as 400 mm

Velocity of flow 0.8 m/s

Head loss due to pipe entry $H = KV^2 / 2g$ 0.017 m

Head loss due to pipe exit

Pipe size considered as 400 mm

Velocity of flow 0.8 m/s

Head loss due to pipe exit $H = KV^2 / 2g$ 0.033 m

Head loss due to orifice

$V = Cd \times (2gh)^{1/2}$

Assume velocity as 0.6 m/s

Cd 0.62

Head loss in orifice 0.05 m

c Head loss due to Filter Outlet Valve (Butterfly valve)

Velocity 0.8 m/s

$h = KV^2 / 2g$

$h = 0.3 \times 0.8^2 / (2 \times 9.81)$ 0.010 m

Head loss due to outlet valve 0.010 m

d. Head Loss in the Filter Bed

Initial Head Loss of Filter : (Ref: CPHEEO Manual)

For Design purpose sieve analysis of filter sand is considered as follows

Sand size, mm	0.3	0.4	0.5	0.6	0.7	0.8	1.0	1.45
% Sand smaller than stated size	0.0	2.0	10	27	50	70	90	100

Porosity of sand bed considered 0.4

Sphericity of sand 1.0



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Head loss for a clean filter is determined using Kozeny's equation for stratified beds

$$\frac{h}{l} = \frac{kV}{g} \frac{(1-f)^2}{f^3} \left[\frac{6}{\phi} \sum_{i=1}^n \frac{P_i}{d_i^2} \right]$$

Where,

h = head loss in m

l = depth of sand bed

0.6 m

K = Carman Kozeny constant

5

V = Velocity of filtration

0.0167 cm/s

v = Kinematic viscosity of water

1.01E-02 cm²/s

f = porosity of clean bed

0.4

Ψ = grain sphericity

1

P_i = Fraction of sandd_i = geometric mean diameter of sand

Size of sand	% of sand larger than stated size	Sand fraction within adjacent sieve size p _i x100	d _i	100	cm x	$\frac{P_i}{d_i^2}$
0.3	0	2	3.5			16
0.4	2	8	4.5			40
0.5	10	17	5.5			56
0.6	27	23	6.5			54
0.7	50	20	7.5			36
0.8	70	20	9			25
1	90	10	12			7
1.4	100	0	-			-
		100				234

h/l = 0.041 m

h = 0.03 m

Hence Total Head Loss

0.235 m

Top level of the sand is considered as 150 mm less than the Weir Level

279.86 m

However for dirty condition of bed a maximum head loss of 1.8 m is considered, before backwash.

1.8 m ✓

Hence TWL of the Filter Bed is

281.66 m

Bottom of the Trough Level considered 150% expansion & Slab thickness of trough

280.31 m

Top of the Trough level considering 0.3m depth

280.61 m

3 Head loss in Filter Inlet Gate and Channel around Filters:

a. Head loss at Inlet Gate to Filters :

Flow to each filter

362.3 m³/hr



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JOB NO	LE150883	TITLE	HYDRAULIC CALCULATIONS	Approved By	BRJ	
Velocity of flow					0.10 m ³ /s	
Area required					1 m/s	
Sluice Gate size			350mm x 350mm		0.10 m ²	
Area of opening					350 mm	
Velocity Provided					0.12 m ²	
Head loss through gate $H = KV^2/2g$					0.8 m/s	
				K	0.62	
				Head loss h	0.022 m	
b. Head Loss in Filter Inlet Channel (FIC):						
No. of filters (twin beds) of FIC					6.00 nos	
Design flow of channel with 20% overloading					0.23 m ³ /s	
Channel size selected						
				Width of Channel	0.40 m	
				Liquid Depth of Channel	1.45 m	
Velocity of Water					0.50 m/s	
For estimation of length maximum length of channel around the filter beds considered.						
Length considered for head loss					78.0 m	
Using Manning's formula, n for concrete					0.014	
				slope, S	0.00050	
Total loss of head					0.039 m	
c. Head loss due to 90° turn						
				for k	0.75	
			headloss	$=0.75 \times 0.5^2 / (2 \times 9.81)$	0.010 m	
				No of bends	1	
				Head loss	0.010 m	
				Total losses	0.071 m	
					281.73 m	
However the TWL of FIC is provided as					281.76 m	
Depth of Filter Inlet Channel					1.45 m	
Invert Level of FIC is provided as					280.31 m	
4 Head loss in Clariflocculator						
Head loss through Clarified Water Common Channel						
Water flow					0.48 m ³ /s	



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CONSULTANT				Prepared By	SRV /-A	Checked By	VVK
JOB NO	LE150883	TITLE	HYDRAULIC CALCULATIONS	Approved By			BRJ
Channel size provided							
Width of Channel						0.75 m	
Liquid depth of channel						0.75 m	
Velocity						0.85 m/s	
Length of Channel from Layout						14 m	
Using manning's equation with n for concrete as						0.014	
				Slope,S		9.077E-04	
				Loss of head		0.013 m	
				Total head loss provided		0.013 m	
TWL of Clarified Water Channel						281.78 m	
However, TWL of Clarified Water Channel provided is						281.81 m	
Depth of Clarified Water Channel						0.75 m	
Invert level of Clarified Water Channel						281.06 m	
b. Head loss in Clarifier Orifice							
Outlet flow from the Clariflocculator						1685.45 m ³ /hr	
Weir length required						141.71 m	
Peripheral orifices of submerged condition							
$V=Cdx(2gh)^{1/2}$							
Assume velocity as						0.6 m/s	
Cd						0.62	
Head loss in orifice						0.05 m	
c. Head loss through Launder							
Overflow per half launder						842.73 m ³ /hr	
						0.23 m ³ /s	
Discharge per unit width of launder, "q"						0.4 m ³ /s	
Critical depth at the end of launder $y_2=[(q/b)^2/g]^{1/3}$						0.36 m	
No. of sides the orifice receives the flow (inside peripheral)						1 no	
Average length of overflow channel from upper to lower end, L						70.9 m	
Discharge per unit length of launder						0.006 m	
Liquid depth at the upper end of the launder, $y_1= [y_2^2+2\{qLN\}^2/(gb^2y_2)]^{1/2}$						0.45 m	
Average liquid depth						0.41 m	
Liquid Depth of launder						0.55 m	
Launder Width						0.6 m	
C/s area of flow						0.246 m ²	
Wetted Perimeter						1.42 m	
Hydraulic mean depth R= A/P						0.17 m	
Manning's coefficient,n						0.014	



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Velocity in launder $V = 1/n R^{2/3} S^{1/2}$					0.59	m/s
Carrying capacity of the Launder					0.145	m ³ /s
The above selected launder size is adequate for carrying capacity indicated above						
Head Loss in the launder					0.05	m
Provided free fall of 0.5m					0.50	m
However Provided WL in the launder at High Point					282.41	m
IL of overflow launder at the High point					281.86	m
IL of overflow launder at the Low point					281.81	m
Provided TWL of Launder at low point					282.36	m
d Head loss due to Central Column						
			$Q = CA (2gh)^{0.5}$			
Flow through central column					1718	m ³ /hr
					0.48	m ³ /s
C value to be considered					0.62	
Area through openings					0.97	m ²
Velocity through opening					0.495	m/s
Head loss through central column					0.03	m
Provided Head loss					0.1	m
Consider 0.1 m losses for Flocculator					0.1	m
TWL of Clarifier required					282.61	m
Liquid Depth of Clarifier					3.0	m
Invert level of Clarifier provided					279.61	m
Invert level of Clarifier at bottom of sludge provided					277.51	m
5 Head Loss between Flash Mixer to Clarifier						
The head loss is mainly due to:						
a. Friction Loss in Inlet pipe to clarifier						
b. Other losses due to Gate/ valve						
a. Head loss through Inlet Pipe						
Size of inlet pipe				DN 900	0.9	m
Head loss as per modified Hazen William's formula'						
$h = \frac{L \left(\frac{Q}{C_R} \right)^{1.85}}{994.62 D^{4.87}}$						
Equivalent Length of pipe including bends(L)					30	m
Flow (Q)					1722.5	m ³ /hr
					0.48	m ³ /s



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CONSULTANT				Prepared By	SRV /ll	Checked By	VVK
JOB NO	LE150883	TITLE	HYDRAULIC CALCULATIONS	Approved By			BRJ
	Roughness coefficient for DI pipe, C_R						1
						head loss, h	0.013 m
	b. Head loss due to Entry and Exit of pipe						
						$HL(f) = KV^2 / 2g$	
	$K = 0.5+1 = 1.5$						
	Head loss due to fittings						0.02 m
	c. Head loss due to fittings						
						$HL(f) = KV^2 / 2g$	
	$K = 0.75$						
	Head loss due to entry and exit of pipe						0.01 m
							0.04 m
	TWL of Flash Mixer arrived						282.76 m
	Depth of Flash Mixer						3.5 m
	Invert level of Flash Mixer						279.26 m
	6 Head loss between Flash mixer and Parshall Flume						
	PARSHALL FLUME:						
	Number of Parshall Flume to measure the flow						1.00 No.
	Flow, Q, design						1718.18 m ³ /h
	=						0.48 m ³ /s
	Flow, Q, Minimum						1718.18 m ³ /hr
	Throat width, W						0.45 m
	=						0.45 m
	Min. flow through the selected throat width						0.0450 m ³ /s
	=						162.00 m ³ /h
	Max. flow through the selected throat width						0.63 m ³ /s
	=						2268.00 m ³ /h
	Discharge equation for the selected throat width : $Q (m^3/s) = 1.038H^{1.537}$						
	Liquid depth Upstream, H						0.6 m
	Liquid depth Downstream, $h=0.6H$						0.36 m
	Length of Parshall Flume for the above selected throat width						
	Axial length of converging section (I1)						1.43 m
	Rise in floor level at the inlet of converging section at slope 1:5						0.29 m
	Length of throat (F) (as per table 1.1)						0.60 m
	Length of diverging section (G) (As per Table 1.12)						0.92 m
	Actual length of flume						2.95 m
	Width of upstream end of the flume (D) (as per table 1, b1)						1.02 m

  L&T Construction <small>WATER, SMART WORLD & COMMUNICATION</small>	
WET 58G	
HYDRAULIC CALCULATIONS-30 MLD WTP ASIFABAD SEGMENT IN ADILABAD DISTRICT	
PROJECT	Providing drinking water to habitations in KomaramBheem-Asifabad Segment in Adilabad district 30 MLD WTP
CLIENT	Govt. of Telangana Rural Water Supply & Sanitation Department
CONSULTANT	M/s. S.K. Associates * HYD-8 *
JOB NO	LE150883
TITLE	HYDRAULIC CALCULATIONS
DRAWING/DOCUMENT NO	LE150883-P-WS-WT-BE-2001
DATE	28.01.2016.
REV B	Sheet 35
Prepared By	SRV <i>f.a.</i>
Checked By	VVK
Approved By	BRJ
head loss	0.59 m
Head required	4.76 m
For ensuring proper backwash the head has been considered as	9 m
Hence Bottom Level of Backwash Overhead Tank	288.86 m
TWL of the Backwash Overhead Tank	291.86 m

"Designs Vetted"



[Signature]
Asst. Executive Engineer
 TDWSP Asifabad

[Signature]
Dy. Executive Engineer
 TDWSP Asifabad

[Signature]
Executive Engineer
 TDWSP Asifabad

"APPROVED"

[Signature]
SE, TDWSP
NIRMAL

CHAPTER - 6

RAW WATER ANALYSIS REPORT

Government of Telangana
State Level Water Quality Monitoring Laboratory
(Rural Water Supply & Sanitation Department)
Hyderabad

Report on Chemical Analysis of Water (Drinking)

Received from : Dy. Executive Engineer, RWS&S, Sub-Division, Mancherla, Adilabad

Date Received : 09.03.2015

Lab Ref. No. : 123 & 124

Particulars of the Sample :

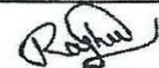
Sample 1 : Ellampally Project, Mancherla (Mandal) Adilabad (District)

Sample 2 : Komaram Bheem Project, ADA, Asifabad (Mandal) Adilabad (District).

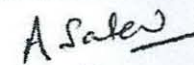
Sl.No.	Physico-Chemical Parameters	Units	Sample Results 1	Sample Results 2	As per BIS (10500 - 2012)	
					Acceptable Limit	Permissible Limit
1	Colour	Co-Pt	Nil	Nil	5	15
2	Turbidity	NTU	Nil	Nil	1	5
3	pH		8.5	8.5	6.5	8.5
4	Electrical Conductivity	micromhos/cm	303	434	-	-
5	Total Dissolved Solids	mg/lit	197	282	500	2000
6	Total Alkalinity as CaCO ₃	mg/lit	62	68	200	600
7	Total Hardness as CaCO ₃	mg/lit	83	120	200	600
8	Calcium as Ca	mg/lit	13	19	75	200
9	Magnesium as Mg	mg/lit	12	18	30	100
10	Flouride as F ⁻	mg/lit	0.29	0.63	1.0	1.5
11	Chloride as Cl ⁻	mg/lit	37	53	250	1000
12	Nitrate as NO ₃	mg/lit	3.7	5.4	45	45
13	Sulphate as SO ₄ ⁻	mg/lit	12.8	18.3	200	400
14	Phosphate as PO ₄ ⁻	mg/lit	0.6	0.8	-	-
15	Sodium as Na	mg/lit	18	45	-	-
17	Potassium as K	mg/lit	2	3	-	-
	Metals					
15	Iron as Fe	mg/lit	0.0789	0.0989	0.1	0.3
18	Manganese (Mn)	mg/lit	0.005	0.0224	0.10	0.30
19	Copper (Cu)	mg/lit	0.0001	0.0001	0.05	1.5
20	Zinc (Zn)	mg/lit	0.0027	0.0032	5.0	15
21	Cadmium (Cd)	mg/lit	0.0003	0.004	0.003	0.003
22	Chromium (Cr)	mg/lit	0.0229	0.0183	0.05	0.05
23	Lead (Pb)	mg/lit	0.0073	0.0044	0.01	0.01
24	Arsenic (As)	mg/lit	0.0001	0.0001	0.01	0.05
24	Pesticides	No pesticide residues are found in water sample				

Remarks : Sample 1: The Chemical Parameters of the above water Sample is Chemically Satisfactory.

Sample 2: The Chemical Parameters of the above water Sample is Chemically Satisfactory.


Analyst


Asst. Chemist
State Level Laboratory


Chemist
State Level Laboratory




WET SBG



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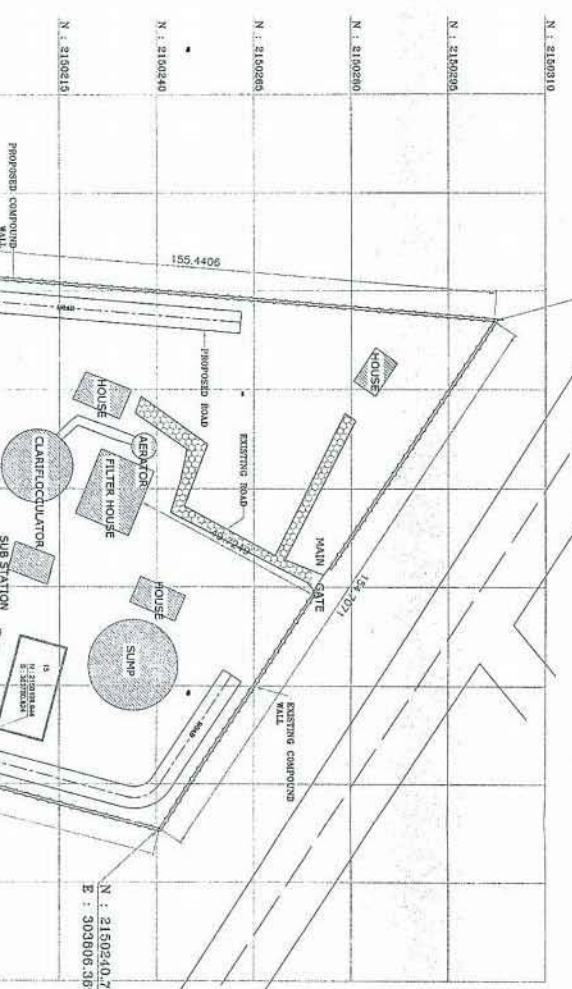
PROJECT	Providing drinking water to habitations in KomaramBheem-Asifabad segment in Adilabad district - 30 MLD WTP	DATE	28.1.2016
SUBJECT	Approval for BEP - LE150883-P-WS-WT-BE-2001 Layout Plan for 30 MLD WTP - LE150883 - P-WS-WT-PP-2002 Hydraulic flow diagram for WTP LE150883 - P-WS-WT-HF-2003 Process flow diagram -LE150883 - P-WS-WT-PF-2004	PAGE	Sheet
Sl.No	Consultant Comments	Reply of L&T	
	Basic Engineering Package for Water treatment Plant (Doc no: LE150883-P-WS-WT-BE-2001) Rev A.		
	The above document revised with the following comments with reference to the Consultant Comments mail dated 25.1.2016 and subsequent telephonic discussion with the consultant dated 28.1.2016.		
1	At Aerator no. of steps to be provided 4nos instead of 3nos to increase the surface loading area.	Noted. Revised BEP (Rev.B) submitted.	
2	Velocity to be considered 0.7m/s instead of 0.9m/s in Aerator launder & Channels.	At Normal Flow Condition the velocity considered for the channel & launder is 0.7m/s and at 20% Overloading Condition the velocity is 0.9m/s.	
3	Retention time to be provide 30mins instead of 25mins in Clariflocculator.	As per Consultant comments mail dt:25.1.2016. and telephonic discussion with consultant the Retention time of flocculator is revised from 25minutes to 30 minutes and the Surface Loading Rate of Clarifier is revised from 35m ³ /day/m ² to 40m ³ /day/m ² and the revised BEP (REV.B) submitted.	
4	Depth of filter sand to be cross checked again with ref standards/codes.	The Provided depth of the filter sand (0.6m) is within in the range of as per the CPHEEO manual on Water Supply and Treatment.	
 Checked by 28/1/2016.			

Chapter- 7

DRAWINGS



TO JAINOOR
 N : 2150326.748
 E : 303677.738



FROM KOMARUM BHEEM DAM
 ADA PROJECT

"Drawings Vetted"
 M/s. S.K. Associates
 HYD & CIVIL
 N : 2150040.538
 E : 303621.636



N : 2150015
 N : 2150100
 N : 2150215
 N : 2150340
 N : 2150280
 N : 2150280
 N : 2150280
 N : 2150310

E : 303645
 E : 303670
 E : 303695
 E : 303720
 E : 303745
 E : 303770
 E : 303795
 E : 303820
 E : 303845

158.2013
 155.4406
 152.7071
 157.1127

Asst. Executive Engineer
 TDWSP Asifabad

SE, TDWSP
 NIRMAL

Executive Engineer
 TDWSP Asifabad

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LIST OF CIVIL UNITS

S.No	DESCRIPTION	QTY	DIMENSION IN METERS
1	Decorative staircase (including handrail)	1	1.50 x 1.50 (sqm)
2	Staircase concrete	1	2.00 x 2.00 x 2.00 (cubic m)
3	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
4	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
5	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
6	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
7	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
8	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
9	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
10	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
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13	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
14	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)
15	Welding channel / REINFORCING TIE	1	1.00 x 0.50 x 0.50 (cubic m)

- NOTES:
- 1) ALL DIMENSIONS ARE (UNLESS SHOWN) IN METERS UNLESS OTHERWISE SPECIFIED.
 - 2) SPACE PROVIDED FOR CASTER ROADMEN HAVE NOT BEEN CONSIDERED & SAME ARE LEFT OPEN.
 - 3) Scaffolding / Formwork.
 - 4) Cement Sandpaper.
 - 5) Existing W.P. STRUCTURES.
 - 6) Existing ROAD.

- REFERENCE DOCUMENTS:
1. CONTRACT DOCUMENT OF KOMARUM-BHEEM DAM
 2. AS PER DRAWING FOR WATER TREATMENT PLANT
 3. LOCAL ESTIMATE-1/10/18-2018
 4. MECHANICAL DRAWING FOR WATER TREATMENT PLANT
 5. DRAWING: 1/10/18-2018

REVNO	DESCRIPTION	DATE	BY	CHECKED
A	FOR APPROVAL	15/09/2018		

L&T Construction
 Water, Smart World & Communication.

CLIENT: RURAL WATER SUPPLY AND SANITATION DEPARTMENT, TELANGANA.
 PROJECT: PROVIDING DRINKING WATER TO HABITATIONS IN KOMARUM-BHEEM ASIFABAD SEGMENT IN ADILABAD DISTRICT (30 MLD WTP)

SUPPLIER/CONTRACTOR: L&T Construction
 WATER & EFFLUENT TREATMENT SFG

JOB NO: LE150803
 TITLE: LAYOUT PLAN FOR WTP

SCALE: 1:500

DATE: 15/09/2018

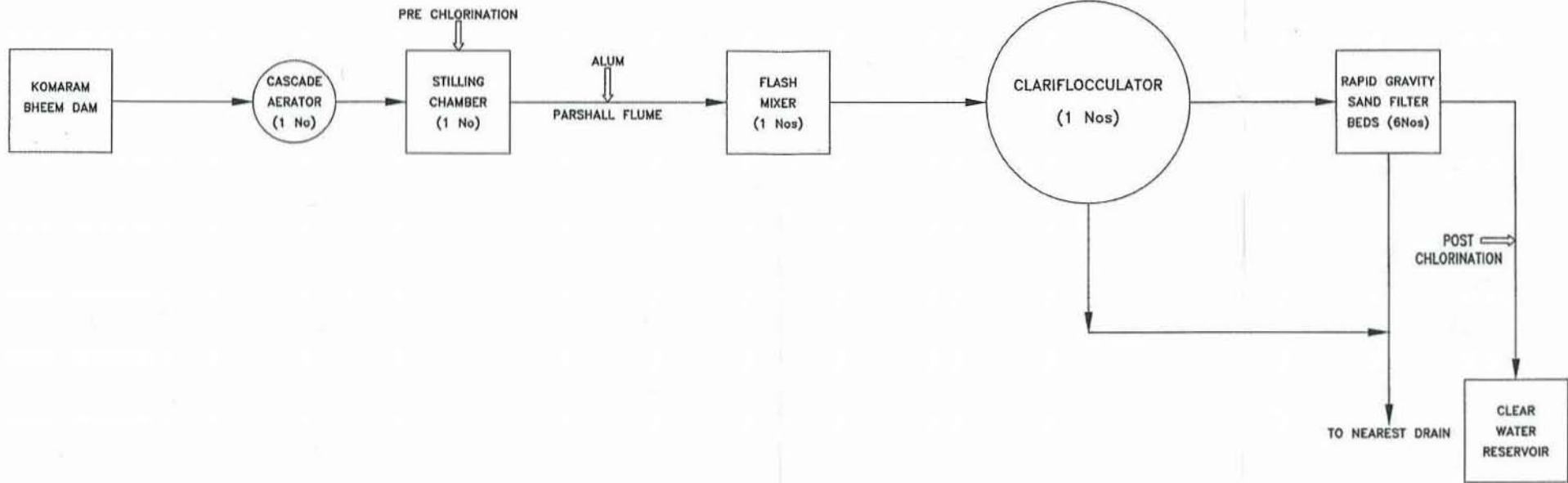
DESIGN: S.V. SIVU
 DRAWING: S.V. SIVU
 CHECK: S.V. SIVU
 APPROVED: S.V. SIVU

DRAWING NO: [E][1][0][8][9][3]-[P]-[W][S]-[W][T]-[P]-[P]-[2][0][10][2]

PREPARED FOR: [] CHEMICAL [] ELECTRICAL [] MECHANICAL [] CIVIL [] CONSTRUCTION

CHECKED BY	DATE	SCALE
CIVIL & STRUCTURAL	15/09/2018	1:500
Mechanical		
Electrical		
Instrumentation		

This drawing is the property of L&T Construction and must not be loaned on to any person or body not authorized by us to receive it nor be copied or otherwise made use either in full or in part by such person or body without our prior permission in writing



"Drawings Vetted"



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Asst. Executive Engineer
TDWSP Asifabad

[Signature]
Dy. Executive Engineer
TDWSP Asifabad

[Signature]
Executive Engineer
TDWSP Asifabad

"APPROVED"
[Signature]
SE, TDWSP
NIKMAL

- REFERENCE DOCUMENT/DRAWINGS :**
1. CONTRACT DOCUMENT OF KOMARAMBHEEM-ASIFABAD SEGMENT IN ADILABAD DISTRICT.
 2. BASIC ENGINEERING PACKAGE FOR WATER TREATMENT PLANT DOC.NO. LE150883-P-WS-WT-BE-2001



A	FOR APPROVAL	SRV/28.12.15	ASA/28.12.15	VVK/28.12.15	BRJ/30.12.15
REV.NO.	DESCRIPTION	DESIGNED	DRAWN	CHECKED	APPROVED

REVISIONS

L&T Construction
Water, Smart World & Communication.

CLIENT : RURAL WATER SUPPLY AND SANITATION DEPARTMENT, TELANGANA. CONSULTANT :

PROJECT : PROVIDING DRINKING WATER TO HABITATIONS IN KOMARAMBHEEM ASIFABAD SEGMENT IN ADILABAD DISTRICT (30 MLD WTP)

SUPPLIER/CONTRACTOR : **L&T Construction**
Water & Effluent Treatment SBG

JOB No :	LE150883	TITLE :	SCALE
NAME	SIGN	DATE	NTS
DSGN SRV	<i>[Signature]</i>	28.12.15	PROJECTION
DRWN ASA	<i>[Signature]</i>	28.12.15	
CHKD VVK	<i>[Signature]</i>	28.12.15	
APPD BRJ	<i>[Signature]</i>	30.12.15	

PROCESS FLOW DIAGRAM OF WTP [30 MLD]

CHECKED BY	SIGN	DATE
CIVIL & STRUCTURAL		
MECHANICAL		
ELECTRICAL		
INSTRUMENTATION		

DRAWING No. **LE150883-P-WS-WT-PF-2004** SIZE **A3** REV. **A**

RELEASED FOR PRELIMINARY TENDER INFORMATION APPROVAL CONSTRUCTION

